



Susol
Super Solution

Low voltage circuit breakers

LS is

Susol MCCB for DC Application

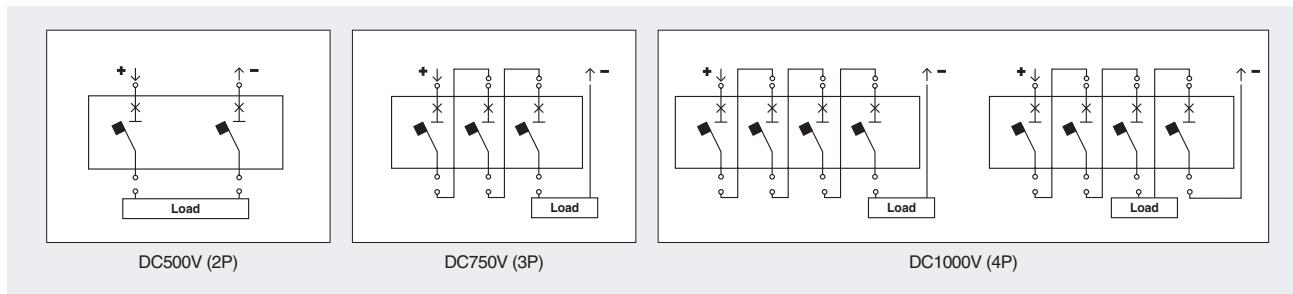
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- Susol MCCB is suitable for DC application such as Photovoltaic Circuit Breaker, UPS and datacenter
- DC short circuit test tested by VDE
- Higher nominal voltage range up to 1000 VDC
- Rated Current : 16A~800A
- No of Pole: 2/3/4Pole
- Available for AC/DC application



		TD100	TD160	TS100	TS160	TS250	TS400	TS630	TS800
Frame size	(AF)	100	160	100	160	250	400	630	800
Rated current, In(A)		16, 20, 25, 32, 40, 50, 63, 80, 100	100, 125, 160	40, 50, 63, 80, 100	100, 125, 160	125, 160 200, 250	300, 400	500, 630	700, 800
No. of Poles	(Pole)	2, 3, 4	2, 3, 4	2, 3, 4	2, 3, 4	2, 3, 4	2, 3, 4	2, 3, 4	2, 3, 4
Rating (DC)	1000V	4P	4P	4P	4P	4P	4P	4P	4P
	750V								
	500V	3P	3P	3P	3P	3P	3P	3P	3P
		2P	2P	2P	2P	2P	2P	2P	2P
Rated service breaking (DC)	Type	N H L N H L N H L N H L N H L N H L N H L							
	1000V (4P)	42 65 100 42 65 100 50 85 100 50 85 100 50 85 100 50 85 100 50 85 100 50 85 100							
	750V (3P)	42 65 100 42 65 100 50 85 100 50 85 100 50 85 100 50 85 100 50 85 100 50 85 100							
	500V (2P)	42 65 100 42 65 100 50 85 100 50 85 100 50 85 100 50 85 100 50 85 100 50 85 100							
Trip unit									
	FTU (fixed-thermal, fixed-magnetic)	● ●							
	FMU (adjustable-thermal, fixed-magnetic)	● ●							
	ATU (adjustable-thermal, adjustable-magnetic)	- -							

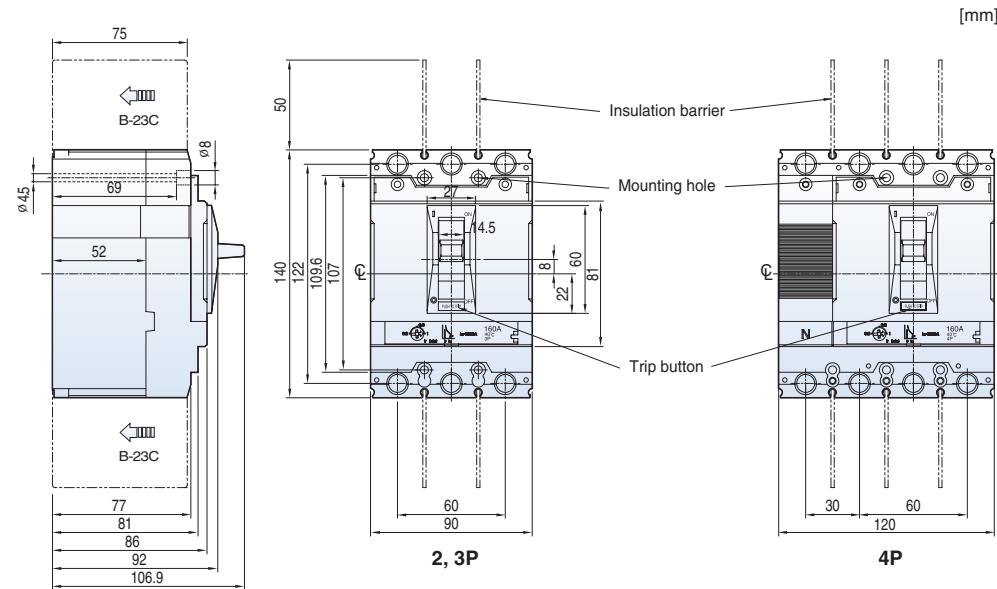
Exemplary circuit diagrams



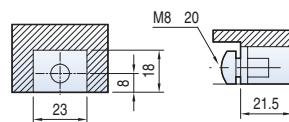
Overall dimensions

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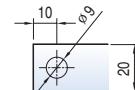
TD100/160



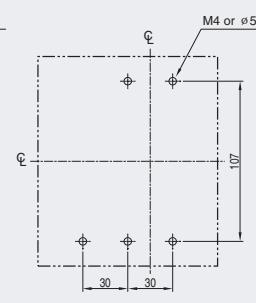
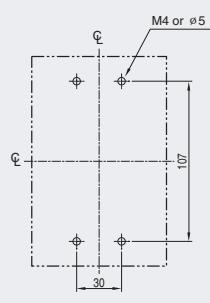
Terminal section



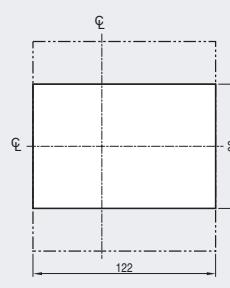
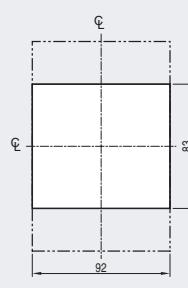
Conductor



Panel drilling



Front panel cutting

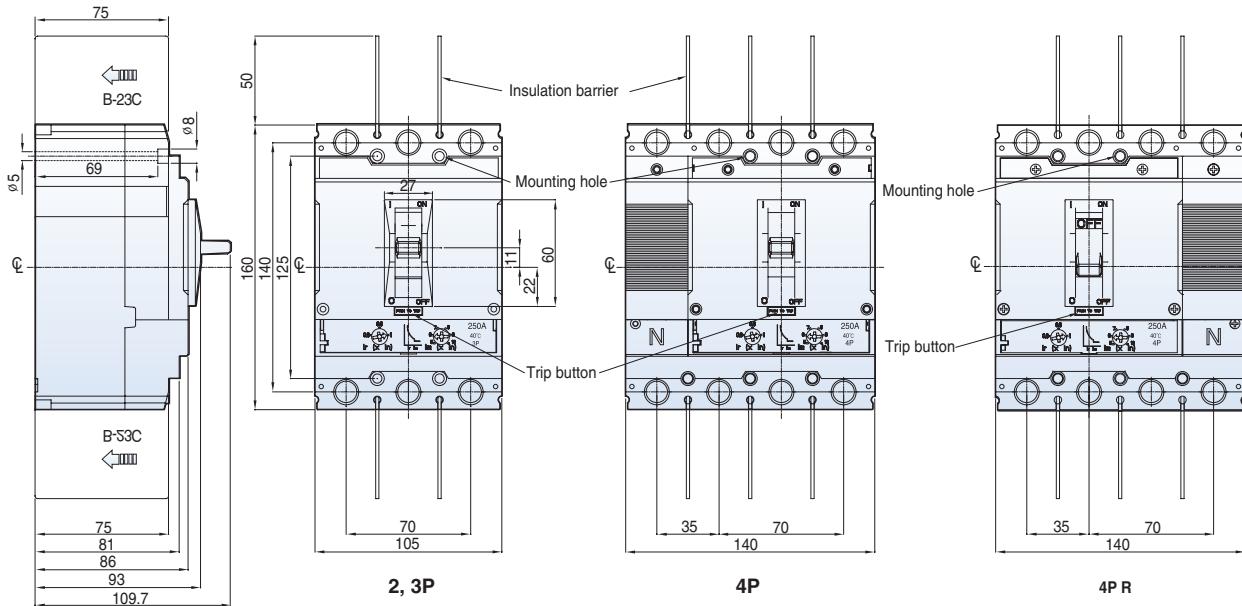


Overall dimensions

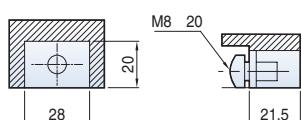
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TS100/160/250

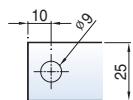
[mm]



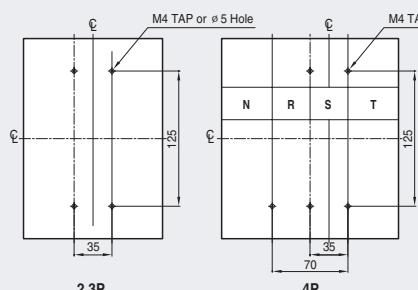
Terminal section



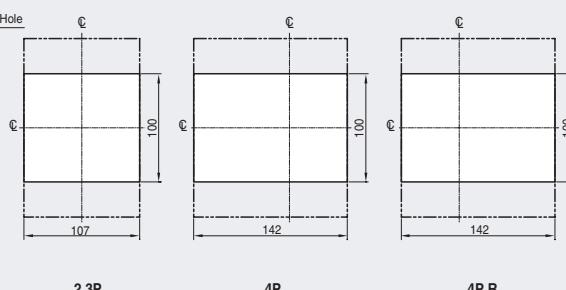
Conductor



Panel drilling



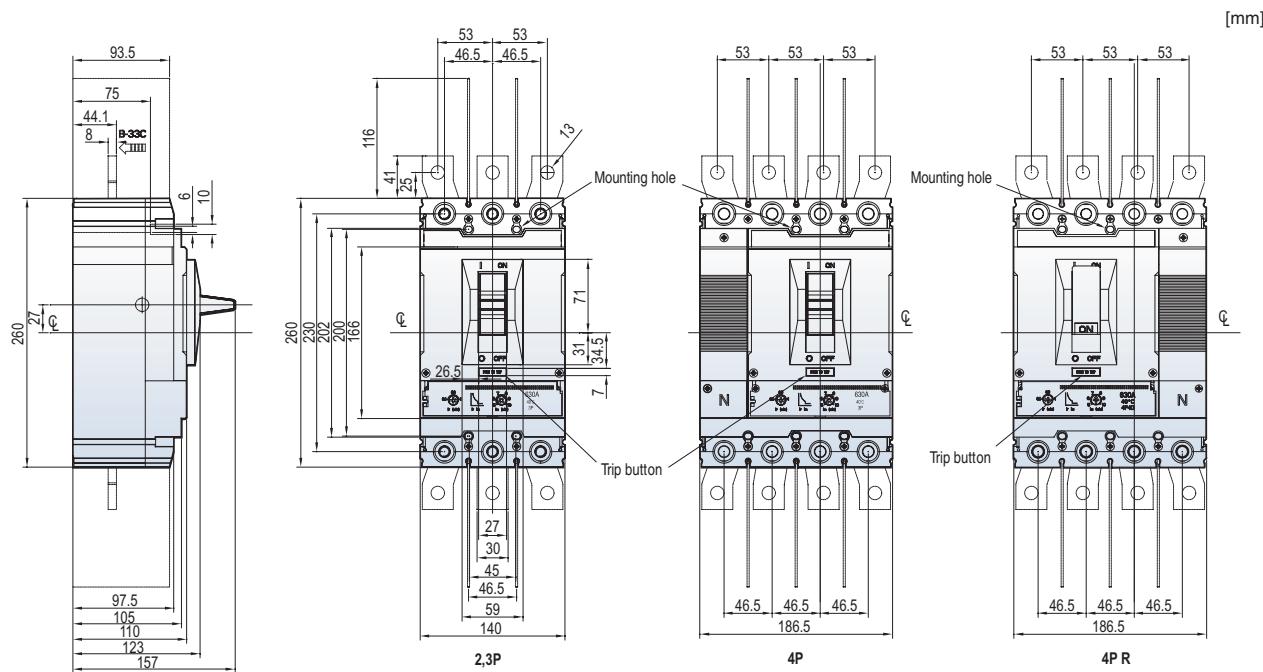
Front panel cutting



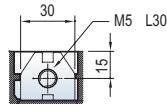
Overall dimensions

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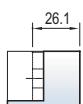
TS400/630



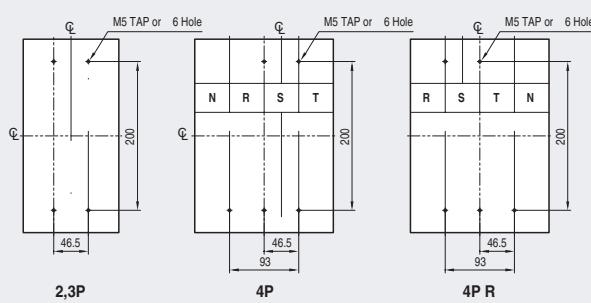
Terminal section



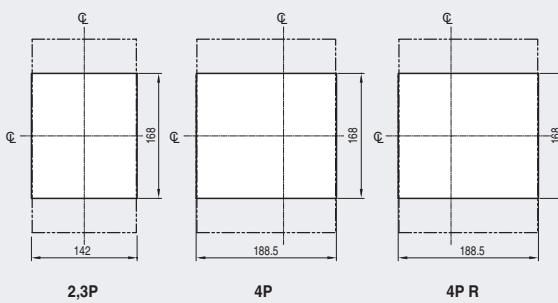
Conductor



Panel drilling



Front panel cutting



Technical information

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How to calculate short-circuit current value Various short-circuit

The purpose of calculating short circuit values

- Selection of circuit breakers, fuse.
- Adjusting metering devices
- Consideration for mechanical resistance
- Consideration for thermal resistance

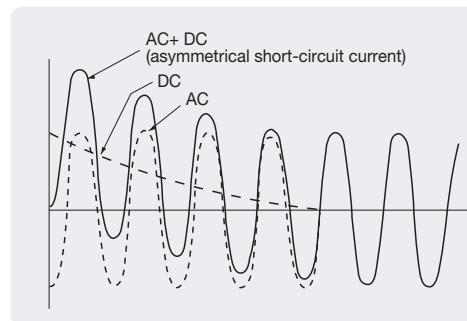
Various value of short-circuit current should be applied to the tests for upper factors.

Symmetrical current for AC and asymmetrical current for DC are used for classifying short circuit current.

Their differences should be essentially considered in the basic step of making network plan.

Symmetrical short-circuit current real value

Short-circuit current is composed of AC and DC as it shows on <Fig.1>. The short-circuit which indicates the real value of AC is called as symmetrical short-current real value, $I_{(rms)sym}$. This current is the essential factor of selecting MCCB, ACB, fuse.



<Fig.1> Composition of short-circuit current

Maximum asymmetrical short-circuit current real value: $I_{(rms)asym}$

The short-circuit which indicates the real value of DC is called as asymmetrical short-circuit current real value.

And this current value is changeable upon the short-circuit closing phase.

This current value is treated for checking the thermal resistant strength of wrings, CT and etc.

With symmetrical short-circuit current real value and short-circuit power factor, we can achieve the value, α from <Fig.5>.

and maximum asymmetrical short-circuit current real value is calculated with this formula.

$$I_{(rms)asym} = \alpha I_{(rms)sym}$$

3-phases average asymmetrical short-circuit current real value: $I_{(rms)ave}$

Each phase is different in its input current value in 3 phases circuit. So that AC rate for 3 phases is different. This value is the average of asymmetrical short-circuit current of 3 phases.

And with symmetrical short-circuit current real value and short-circuit power factor, we can achieve the value, β , and 3-phases average asymmetrical short circuit current real value is calculated with this formula.

$$I_{(rms)ave} = \beta I_{(rms)sym}$$

Maximum asymmetrical short-circuit current instantaneous value: I_{max}

Each phase has different instantaneous current value. And when asymmetrical short-circuit current shows its maximum instantaneous value, the current value is called as maximum asymmetrical short-circuit current instantaneous value. This current is to test the mechanical strength of serial equipments.

And with symmetrical short-circuit current real value and short-circuit power factor, we can achieve the value, γ and maximum asymmetrical short-circuit current instantaneous value is calculated with this formula.

$$I_{max} = \gamma I_{(rms)sym}$$

Network impedance for calculating short-circuit current value

Bellows should be considered for the calculation as the impedance components affecting circuit to trouble spot from short-circuit power.

a. Primary part impedance of incoming transformer It's calculated from the short-circuit current data which is provided by power supplier. Calculated value can be regarded as reactance.

b. Impedance of incoming transformer Its amount is upon the capacity of transformer and primary voltage. Generally this impedance can be regarded as reactance and refer to <Table.4>, <Table.5>.

Technical information

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How to calculate short-circuit current value Various short-circuit

c. Reactance of motor

Motor works as generator and supply short circuit current in the condition of an accident circuit such as <Fig.2>.

Generation factor of firm motor should be considered in a low voltage circuit where a circuit breaker operates quickly and in a high voltage circuit for the selection of fuse. Reactance of motor can be regarded in the range of 25% normally.

d. Distribution impedance

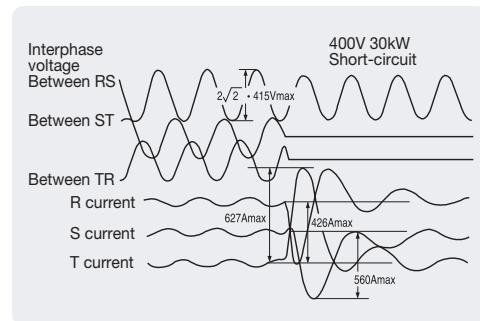
Impedance of cable and busduct do control short-circuit remarkably in low voltage network. Refer to <Table.5>, <Table.6>.

e. Others

MCCB, ACB CT are equipments for the network of low voltage.

The impedance of these equipment which is calculated from short-circuit current value should be considered.

Generally, the impedance of those equipment is that of rated current (normal condition), if operators apply that impedance value, bigger reactance value may be applied to calculated short-circuit current value.



<Fig.2> Short-circuit of motor

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How to calculate short-circuit current value With percent impedance

Ohm formula (Ω), percent impedance formula (%), unit formula (per unit) can be applied to calculate short-circuit current value.

Ohm formula [Ω]

Short-circuit current value is calculated by converting into ohm value [Ω]

Percent impedance formula (%) Each impedance is converted into the impedance of base value and base voltage.

And the required amount for electric demand should be shown as percent unit.
And apply that value in ohm formula.

Unit formula

The base value equals 1.0. and all value of network shows in the way of decimal system. Applying any of upper calculation formulas to achieve short-circuit current value, it shows equal value. To select a certain formula for doing it, operator can select one of those formula which is proper to oneself. Below is percent impedance formula.

Finding base value

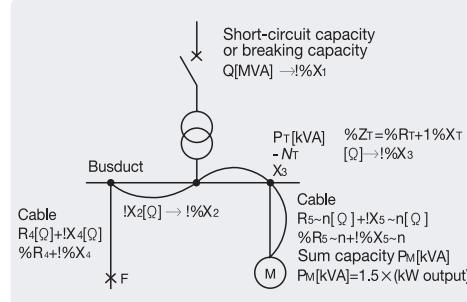
The rated current of transformer shall be the base value.

Base capacity $P_B = P_T$ [kVA]

Base voltage $V_B = V_T$ [V]

$$\text{Base current } I_B = I_T = \frac{P_T}{\sqrt{3}V_T} \times 10^3 [\text{A}]$$

$$\text{Base impedance } Z_B = \frac{V_B^2}{P_B \times 10^3} = \frac{V_T^2}{P_T \times 10^3} [\Omega]$$



<Fig.3> Base value

Converting impedance into base value

a. Primary part impedance of transformer: $%X_1$

$$\%X_1 = \frac{P_B}{Q \times 10^3} \times 100 [\%]$$

Q: Primary part short-circuit capacity

b. Impedance of transformer: $%Z_T$

It generally indicates as percent impedance. If base capacity is equal to transformer capacity, $%ZT$ can be used as it is. When base capacity is not equal to transformer capacity, convert values by this formula.

$$\frac{P_T}{%Z_T} = \frac{P_B}{%Z_B}$$

: value converted by base value

1phase transformer should converted into the value of 3 phase transformer, And the percent impedance is equal to $\frac{\sqrt{3}}{2} \times$ calculated urgent value.

c. Reactance of motor: $%X_m$

Transformer capacity shows the value in kW, so it is converted into unit, kVA.
(kVA value) $\approx 1.5 \times$ (Output of motor, kW)
 $%X_m = 25\%$ Converting it from base capacity

$$\frac{P_m}{%X_m} = \frac{P_B}{%X_B}$$

(Converting formula for different capacity)

d. Impedance of busduct, cable

Cable: Area of cross-section & length
Busduct: Rated current

In <Fig.5>, <Fig.6>

$Z_c = (\Omega \text{ per each unit length}) \times (\text{length}) [\Omega]$
Convert this value into % value.

$$\%Z_c = \frac{Z_c}{Z_B}$$

(% converting formula)

2cables in same dimension, it's recommendable to divide the length by 2.

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How to calculate short-circuit current value

Preparing a impedance map

Prepare impedance map according to the impedance value from (2). Various electricity suppliers like source, motor have same electric potential in impedance map.

As you find it on <Fig.4> (a), extend it from the unlimited bus to fault point, draw impedance map.

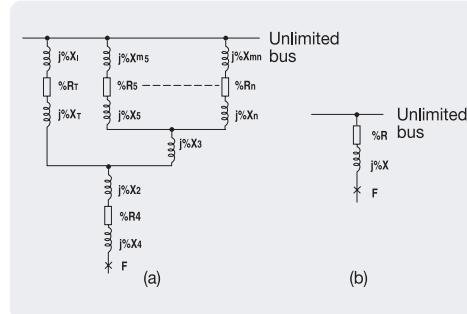
Calculating impedance

Calculate impedance as <Fig.4 (b)> in impedance map <Fig.4 (a)>

$$\%Z = \%R + j \%X$$

$$\%Z = \sqrt{(\%R)^2 + (\%X)^2}$$

Calculating symmetrical short-circuit current real value



<Fig.4> Base value

Calculating various short-circuit current value

$$IF(3\phi) = IF(rms)sym(3\phi)$$

$$= \frac{P_B \times 10^3}{\sqrt{3}V_B \cdot \%Z} \times 100$$

$$= \frac{I_B}{\%Z} \times 100 [A]$$

Calculate various short-circuit current value with α , β , γ values from <Fig.5> like

$$\text{short-circuit power factor cos } \phi = \frac{\%R}{\%Z}$$

3 phases average asymmetrical real value

$$I_F(rms)ave = \beta I_F(rms)sym$$

Maximum average asymmetrical real value

$$I_F(rms)asym = \varrho I_F(rms)sym$$

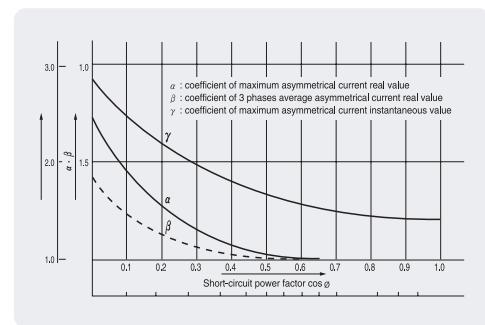
Maximum asymmetrical instantaneous value

$$I_Fmax = \gamma I_F(rms)sym$$

In case of 1 phase short-circuit

$$\text{Current value from (5) multiplied by } \frac{\sqrt{3}}{2}$$

$$\text{Each short-circuit current value (1\phi)} = \frac{\sqrt{3}}{2} \\ (3\text{phases short-circuit current}) \times \alpha \text{ (or } \gamma \text{)}$$



<Fig.5>

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How to calculate short-circuit current value With a simple formula

For its special cases, calculating exact value should be needed, in the other hand, for the practical use, we recommend simple formula.

Finding a base value

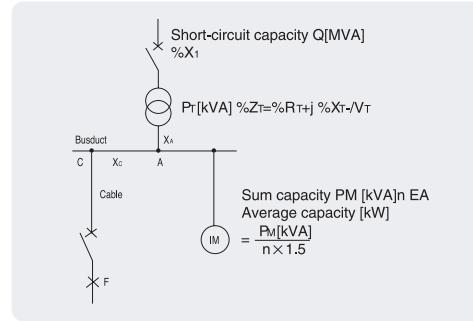
It shall be the rated current of transformer.

$$P_B = PT \text{ [kVA]}$$

$$V_B = VT \text{ [V]}$$

$$I_B = IT \text{ [A]}$$

$$Z_B = \frac{VT_B \text{ [} \Omega \text{]}}{PT \times 103}$$



Short-circuit current from incoming circuit

Disregard the impedance value of primary part of transformer. Calculate short-circuit current value according to <Fig.7>.

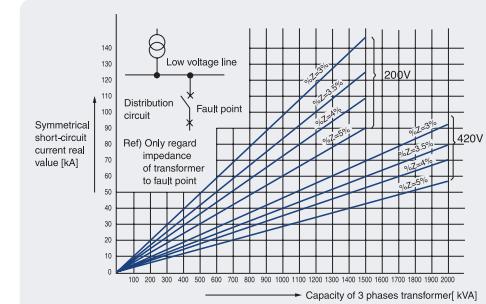
(If the impedance value of primary part of transformer is considered, calculate the current value as below formula)

$$I_A(R) = \frac{I_B}{\sqrt{(\%R_T)^2 + (\%X_t + \%X_T)^2}} \times 100 \text{ [A]}$$

$$\%X_t = \frac{P_B}{Q \times 10^3} \times 100 \text{ [%]}$$

If the value of $\%R_T$ is not clear, $\%Z_t = \%T_T$

$$I_A(R) = \frac{I_B}{\%X_t + \%X_T} \times 100 \text{ [A]}$$



Ref 1) Calculation in the random voltage E Voltage line which is mostly close to E shall be selected to calculate it.

i.e. in case of 220V, (200V line value) ÷ 200/220

Ref 2) Calculation for a certain impedance Z_t (%) Impedance line which is mostly close to Z_t (%) shall be selected to calculate it.

i.e. 420V, $Z_t = 4.5\%$

$\%Z = 4$ Line value (or 5% line) × 4 (or 5)/4.5

Ref 3) When the value is out of lines or over 200VA or below 100kA, multiply 10 times to the calculated values.

<Fig.7> Transformer capacity and short-circuit current

Short-circuit current to motor

$$I_A(M) = 4 \times I_A(R) \text{ (Rated current of motor)}$$

Symmetrical short-circuit current at point A

$$I_A = I_A(R) + I_A(M)$$

Decreasing coefficient caused by busduct

$$\text{Obtaining the value of } \frac{I_A \cdot I_{A_c}}{10V_T}$$

Calculate decreasing coefficient from <Fig.10>

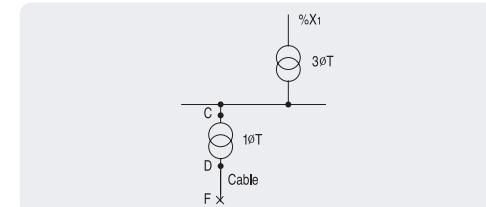
Decreasing short-circuit current by reactance

When there's 1phase transformer in a certain circuit, calculate it in the base of reactance.

Regarding the reactance as pre-impedance at source part at point of <Fig.8>,

$$X_C = \frac{E_B}{\sqrt{3} I_C}$$

Reactance C~D: $X_D \text{ [} \Omega \text{]}$ (impedance of 1 $\emptyset T$)



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How to calculate short-circuit current value

Calculating the value of X_D/X_C and decreasing coefficient d from the reactance of <Fig.9>.

Current at point D $I_D = d \cdot I_C$

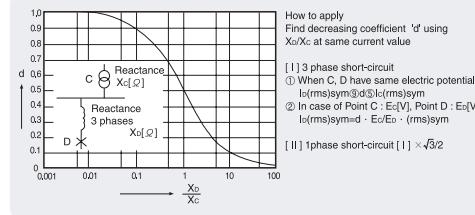
Impedance of 1 phase transformer $X_D = X (1 \text{ } \varnothing) \frac{1}{2}$

a. Short-circuit current at E_C voltage base

$$I_D (\text{rms})\text{sym} \cdot 3 \varnothing = d \cdot I_C (\text{rms})\text{sym} \cdot 3 \varnothing$$

b. Short-circuit current at E_D voltage base

$$I_D (\text{rms})\text{sym} \cdot 3 \varnothing = d \cdot I_C (\text{rms})\text{sym} \cdot 3 \varnothing \times E_C/E_D$$



<Fig.9> Decreasing coefficient of short-circuit current by reactance: d

Coefficient d for cables

Calculating the value of $\frac{l_D}{10V_T} I_D$

Decreasing coefficient b value is calculated from <Fig.13>. For insulator drawn wrings, we can find the value directly from <Fig.13>.

Calculating symmetrical short-circuit current real value

$$I_F (\text{rms})\text{sym} = b \times I_D [D]$$

Various short-circuit current

In case of having short-circuit current power factor, find α, β, γ from <Fig.5>, If not find 3 values from <Table.1>

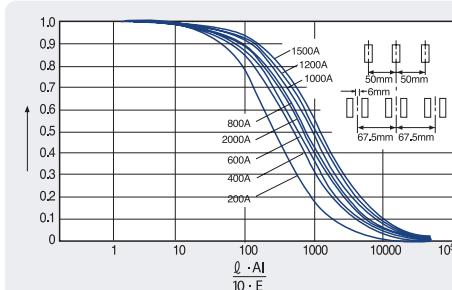
- 3 phases short-circuit asymmetrical current average value
 $I_F (\text{rms})\text{ave} = \beta I_F (\text{rms})\text{sym}$
- Maximum asymmetrical real value
 $I_F (\text{rms})\text{ave} = \alpha I_F (\text{rms})\text{sym}$
- Maximum asymmetrical instantaneous value
 $I_F (\text{rms})\text{ave} = \gamma I_F (\text{rms})\text{sym}$

<Table.2> α, β, γ values when short circuit power factor value is not definite.

Symmetrical short-circuit real value (A)	Variables		
	Maximum asymmetrical real value	3 phases short-circuit asymmetrical current average value	Maximum asymmetrical instantaneous value
2500	1.0	1.0	1.48
2501~5000	1.03	1.02	1.64
5001~10000	1.13	1.07	1.94
10001~15000	1.18	1.09	2.05
15001~25000	1.25	1.13	2.17
25000	1.33	1.17	2.29

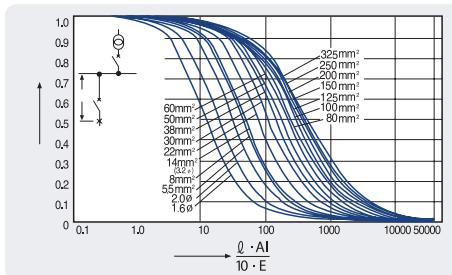
1 phase short-circuit

$$(\text{Each current}) = \frac{\sqrt{3}}{2} \times 3 \text{ phases short-circuit current} \times \gamma \text{ (or } \alpha \text{)}$$

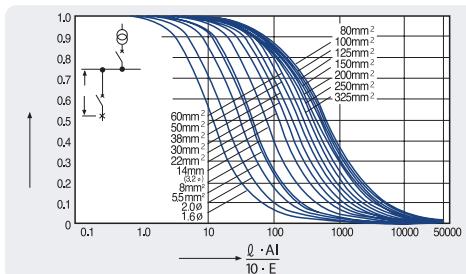


Busduct Ratings (A) Material	General busduct			
	Size [mm] [Ω/m]	Resistance R [Ω/m]	Reactance X [Ω/m]	Impedance Z [Ω/m]
Cu	200	3×25	2.41×10^4	1.312×10^4
	400	6×40	0.751×10^4	1.267×10^4
	600	6×50	0.607×10^4	1.094×10^4
	800	6×75	0.412×10^4	0.72×10^4
	1000	6×100	0.315×10^4	0.60×10^4
	1200	6×125	0.261×10^4	0.516×10^4
	1500	6×150	0.221×10^4	0.449×10^4
	2000	$6 \times 125 \times 2$	0.129×10^4	0.79×10^4
	0.800×10^4			

<Fig.10> Decreasing coefficient of general busduct (Cu)



<Fig.11> Decreasing coefficient b in cable (600V IV)



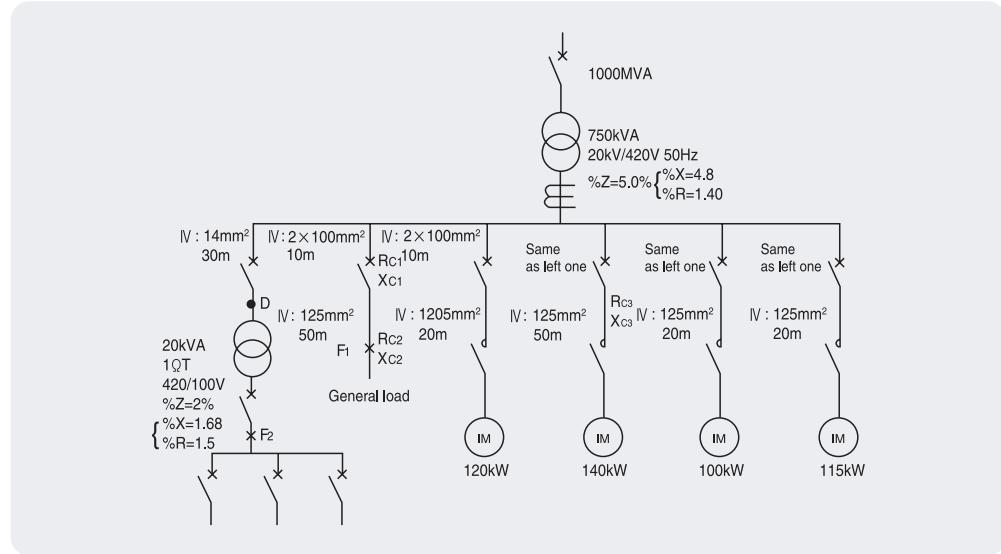
<Fig.12> Decreasing coefficient b in cable (600V IV)

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How to calculate short-circuit current value Calculation example

Calculation1) Short-circuit current value will be achieved by simple formula and percent impedance formula for <Fig.13>



<Fig.13>

Percent impedance formula

(1) Base value

$$P_B = 750 \text{ kVA} \quad V_B = 420 \text{ V}$$

$$I_B = 1031 \text{ A} \quad Z_B = 0.237 \Omega$$

(2) Each impedance

a. Reactance at primary part of transformer

$$\%X_1 = \frac{750}{1000 \times 10^3} \times 100 = 0.075 [\%]$$

b. Impedance of transformer

$$\%R_T = 1.4\%$$

$$\%X_T = 4.8\%$$

c. 1 Ø Tr impedance

$$\%R_{T1} = \frac{1.15 \times 750}{20} \times \frac{1}{2} = 21.6 [\%]$$

$$\%X_{T1} = \frac{1.68 \times 750}{20} \times \frac{1}{2} = 31.5 [\%]$$

d. Reactance of transformer

$$\%X_{m1} = \frac{750}{120 \times 1.5} \times 25 = 104 [\%]$$

$$\%X_{m2} = \frac{750}{140 \times 1.5} \times 25 = 89 [\%]$$

$$\%X_{m3} = \frac{750}{100 \times 1.5} \times 25 = 125 [\%]$$

$$\%X_{m4} = \frac{750}{115 \times 1.5} \times 25 = 108.7 [\%]$$

e. Impedance of cable

Converting impedance of whole metal tube

[2x100mm² 10m]

$$\%R_{c1} = \frac{0.00018 \times 10}{0.237} \times \frac{1}{2} \times 100 = 0.38 [\%]$$

$$\%X_{c1} = \frac{0.00013 \times 10}{0.237} \times \frac{1}{2} \times 100 = 0.27 [\%]$$

[125mm² 20m]

$$\%R_{c2} = \frac{0.00014 \times 20}{0.237} \times 100 = 1.18 [\%]$$

$$\%X_{c2} = \frac{0.00013 \times 20}{0.237} \times 100 = 1.09 [\%]$$

[250mm² 50m]

$$\%R_{c3} = \frac{0.00007 \times 50}{0.237} \times 100 = 1.47 [\%]$$

$$\%X_{c3} = \frac{0.00013 \times 50}{0.237} \times 100 = 2.74 [\%]$$

[14mm² 30m]

$$\%R_{c4} = \frac{0.00013 \times 30}{0.237} \times 100 = 16.45 [\%]$$

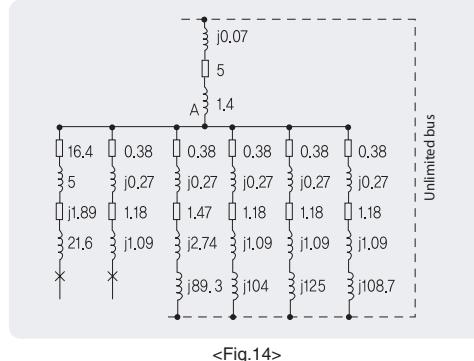
$$\%X_{c4} = \frac{0.00015 \times 30}{0.237} \times 100 = 1.88 [\%]$$

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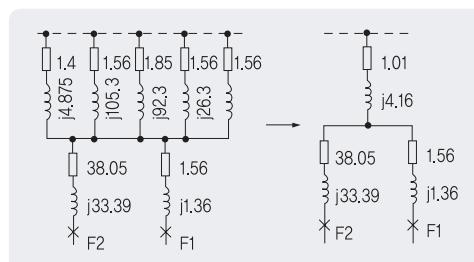
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How to calculate short-circuit current value

- (3) Preparing a impedance map
Connect short-circuit supplier to the unlimited bus.



Calculating impedance
Calculate it in serial/parallel type formula

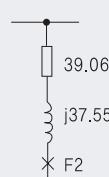


a. Fault point F₁



$$\%Z_1 = \sqrt{(2.57)^2 + (5.53)^2} = 6.1[\%]$$

b. Fault point F₂



$$\%Z_2 = \sqrt{(39.06)^2 + (37.55)^2} = 54.2[\%]$$

- (5) Calculation of asymmetrical short-circuit current

a. Fault point F₁

$$I_{F1} (\text{rms})\text{sym} = \frac{1031}{6.1} \times 100 = 16900 [\text{A}]$$

$$\cos \phi_1 = \frac{2.57}{6.1} = 0.422$$

b. Fault point F₂ (1 phase circuit)

$$I_{F2} (\text{rms})\text{sym} = \frac{1031}{54.2} \times 100 = 1902 [\text{A}] \dots (\text{at } 100\text{V})$$

$$= \frac{1031}{54.2} \times 100 \times \frac{420}{100} = 7989 [\text{A}] \dots (\text{at } 420\text{V})$$

I_{F2} (rms)sym is short-circuit current.
Therefore, convert it into 1 phase short-circuit current.

$$I_{F2} (\text{rms})1 \Omega \text{ sym} = 7989 \times \frac{\sqrt{3}}{2} = 6919 [\text{A}]$$

$$\cos \phi_2 = \frac{39.06}{54.2} = 0.72$$

- (6) Various short-circuit current
Calculate α , β , γ from <Fig.5>.

a. Fault point F₁

$$\cos \phi_1 = 0.422$$

$$\alpha = 1.05 \quad \beta = 1.3 \quad \gamma = 1.74$$

$$I_{F1} (\text{rms})\text{ave} = 1.03 \times 16900 = 17407 [\text{A}]$$

$$I_{F1} (\text{rms})\text{asym} = 1.05 \times 16900 = 17745 [\text{A}]$$

$$I_{F1}\text{max} = 1.74 \times 16900 = 29406 [\text{A}]$$

b. Fault point F₂

$$\cos \phi_2 = 0.72$$

$$\alpha = 1.0 \quad \beta = 1.48$$

$$I_{F2} \text{ (rms)asym} = 1.0 \times 6919 [\text{A}]$$

$$I_{F2} \text{ max} = 1.48 \times 6919 = 10240 [\text{A}]$$

Simple calculation formula

- (1) Base value

$$P_B = 750 \text{kVA} \quad V_B = 420 \text{V}$$

$$I_B = 1031 \text{A} \quad Z_B = 0.237 \Omega$$

- (2) Short-circuit current of incoming circuit

Disregard the impedance of primary part of transformer
In <Fig.7> $I_{A(\text{R})} = 20500 \text{ A}$

- (3) Short-circuit current of motor

$$\text{Sum of motor capacity} = (120+140+100+115) \times 1.5 = 713 [\text{kVA}]$$

$$I_{A(M)} = \frac{713}{\sqrt{3} \times 420} \times 4 = 3920 [\text{A}]$$

- (4) Symmetrical short-circuit current at point A
 $I_A = 20500 + 3920 = 24420 \text{ A}$

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How to calculate short-circuit current value Calculation example

(5) Decreasing short-circuit current for cable

a. At point F₁

- $2 \times 100\text{mm}^2 10\text{m}$
 $2 \times 100\text{mm}^2 10\text{m} = 100\text{mm}^2 5\text{m}$
 $\frac{l}{10E} = \frac{20 \times 24420}{10 \times 420} = 29.1$

Coefficient b= 0.935

Short-circuit current value at point C

$$I_C (\text{rms}) \text{sym} = 0.935 \times 24420 = 22850 \text{ [A]}$$

- $125\text{mm}^2 20\text{m}$
 $\frac{l}{10E} = \frac{20 \times 22850}{10 \times 420} = 108.9$

$$I_{F1} (\text{rms}) \text{sym} = 0.785 \times 244850 = 17940 \text{ [A]}$$

b. At point F₁

- $14\text{mm}^2 30\text{m}$
 $\frac{l}{10E} = \frac{30 \times 24420}{10 \times 420} = 174.4$

Coefficient b= 0.249

$$I_D (\text{rms}) 3\phi \text{sym} = 0.24 \times 24420 = 6080 \text{ [A]}$$

- Decreasing by the reactance ($1\phi Tr$)dp
 Convert the value of '%X of $1\phi Tr$ ' to base capacity
 $X_0 = 750 \times 2/20 = 75\%$
 Impedance of primary part at $1\phi Tr$

$$XA = \frac{I_B}{I_D} \times 100 = \frac{1031}{6080} \times 100[\%]$$

Convert X_D to equivalent 3 phases, and

$$\frac{X_D/2}{X_A} = \frac{750 \times 2 \times 6080}{20 \times 2 \times 1031 \times 100} = 2.21$$

Coefficient d of <Fig.9> d= 0.32

$$I_{F2} (\text{rms}) 3\phi \text{sym} = 0.32 \times 6080 = 1945 \text{ [A]} (400V)$$

$$= 0.32 \times 6080 \times 420/100$$

$$= 817 \text{ [A]} (100V)$$

$$\therefore I_{F2} (\text{rms}) 1\phi \text{sym} = 817 \times \frac{\sqrt{3}}{2} = 7076 \text{ [A]}$$

(6) Various short-circuit current

Find α, β, γ from <Table.1>

a. At point F₁

$$\alpha = 1.25 \quad \beta = 1.13 \quad \gamma = 2.17$$

$$IF1 (\text{rms}) \text{ave} = 1.13 \times 17940 = 20272 \text{ [A]}$$

$$IF1 (\text{rms}) \text{asym} = 1.25 \times 17940 = 22425 \text{ [A]}$$

$$IF1 \text{max} = 2.17 \times 17940 = 38930 \text{ [A]}$$

b. At point F₂

$$\alpha = 1.13 \quad \gamma = 1.94$$

$$IF21 \phi (\text{rms}) \text{asym} = 1.13 \times 7076 = 7945 \text{ [A]}$$

$$IF21 \phi \text{max} = 1.94 \times 7076 = 13727 \text{ [A]}$$

<Table.2> Comparison of short-circuit

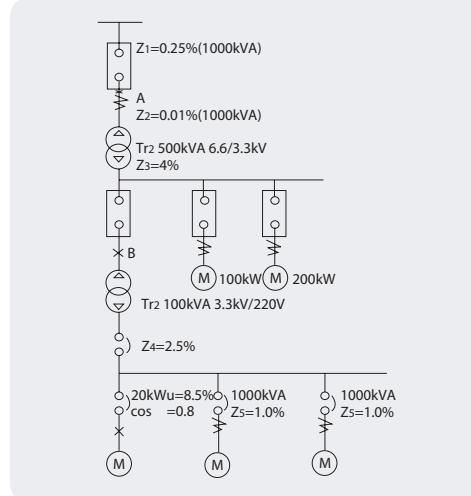
Fault point	F ₁	F ₂
Symmetrical short-circuit current real value	Percent impedance calculation value	16900A
	Simple formula calculation value	17940A
3 phases average asymmetrical current real value	Percent impedance calculation value	7076A
	Simple formula calculation value	106% 102%
Maximum asymmetrical current real value	Percent impedance calculation value	17407A
	Simple formula calculation value	-
	Percent impedance calculation value	20272A
	Simple formula calculation value	116% -
	Percent impedance calculation value	17745A
	Simple formula calculation value	6919A
	Percent impedance calculation value	22425A
	Simple formula calculation value	7995A
	Percent impedance calculation value	126% 115%
	Simple formula calculation value	-

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How to calculate short-circuit current value

Short-circuit current value will be achieved by simple formula for <Fig.16>



<Fig.16>

- (1) Calculate rated current at each point
① Rated current I_{nA} at point A

$$I_{nA} = \frac{500[\text{kVA}] \times 1000}{\sqrt{3} \times 6.6[\text{kV}] \times 1000} = 43.7[\text{A}]$$

- ② Rated current I_{nB} at point B

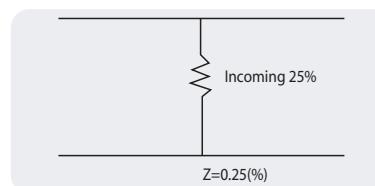
$$I_{nB} = \frac{100[\text{kVA}] \times 1000}{\sqrt{3} \times 3.3[\text{kV}] \times 1000} = 17.5[\text{A}]$$

$$I_{nc} = \frac{20[\text{kW}] \times 1000}{\sqrt{3} \times 220[\text{V}] \times 0.85 \times 0.8} = 77.2[\text{A}]$$

- (2) Put 1000 kVA for base capacity and calculate short-circuit current at each point.

- ① Short-circuit current I_{SA} at point A

- a) Impedance Map



- b) Short-circuit I_{SA}

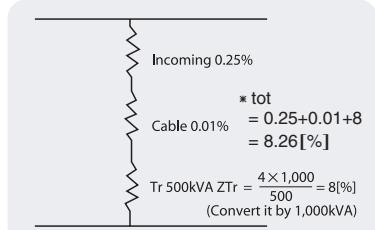
$$I_{SA} = \frac{1000[\text{kVA}] \times 1000 \times 100}{\sqrt{3} \times 6.6[\text{kV}] \times 1000 \times 0.25\%} = 34990[\text{A}]$$

- * Breaking capacity of breaker [MVA]
 $MVA = 3 \text{ short-circuit current[kA]} \times \text{line voltage[kV]}$

- ② Short-circuit current at point B: I_{SB}

- a) Impedance Map

* Serial sum of impedance
 $Z_{\text{tot}} = 0.25 + 0.01 + 8 = 8.26\%[]$



- b) Short-circuit current I_{SC}

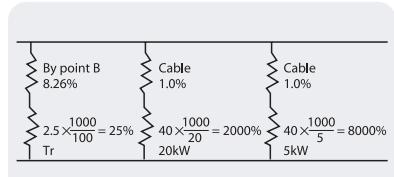
$$I_{SB} = \frac{1000[\text{kVA}] \times 1000 \times 100}{\sqrt{3} \times 3.3[\text{kV}] \times 1000 \times 8.26} = 2118[\text{A}]$$

- * Breaking capacity of breaker [MVA]

$$\text{MVA} = \sqrt{3} \text{ short-circuit current [kA]} \times \text{line to line voltage[kV]}$$

- ③ Short-circuit current at point C: I_{SC}

- a) Impedance Map



- * Parallel sum of impedance

$$Z = \frac{1}{\frac{1}{33.26} + \frac{1}{2001} + \frac{1}{8001}} = 32.58 [\%]$$

- b) Short-circuit current I_{SC}

$$I_{SC} = \frac{1000[\text{kVA}] \times 1000 \times 100}{\sqrt{3} \times 220[\text{V}] \times 32.58[\%]} = 8055 [\text{A}]$$

Calculation formula

$$\text{Rated current } I_n = \frac{\text{Transformer capacity}}{\sqrt{3} \times \text{Rated voltage}}$$

$$\text{Short-circuit current } I_s = \frac{\text{Transformer capacity} \times 100}{\sqrt{3} \times \text{Rated voltage} \times \%Z}$$

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How to calculate short-circuit current value Combination of transformer and impedance

<Table. 3> Combination of transformer and impedance

Transformer Impedance	3 phases transformer											
	6.3kV/210V Oil Tr.			6.3kV/210V Mold Tr.			20kV/420V Mold Tr.			20kV/420V Oil Tr.		
Transformer capacity (VA)	ZT[%]	RT[%]	XT[%]	ZT[%]	RT[%]	XT[%]	ZT[%]	RT[%]	XT[%]	ZT[%]	RT[%]	XT[%]
20	2.19	1.94	1.03									
30	2.45	1.92	1.53	4.7	2.27	4.12						
50	2.47	1.59	1.89	4.7	1.94	4.28						
75	2.35	1.67	1.66	4.4	1.56	4.11						
100	2.54	1.65	1.96	4.6	1.5	4.24						
150	2.64	1.64	2.07	4.2	1.29	4.0						
200	2.8	1.59	2.31	4.5	1.17	4.35						
300	3.26	1.46	2.92	4.5	1.2	4.33						
500	3.61	1.33	3.36	4.7	0.08	4.69	5.0	1.56	4.76	6.0	1.0	5.92
750	4.2	1.55	3.9	6.0	0.8	5.95	5.0	1.40	4.80	6.0	0.9	5.93
1000	5.0	1.35	4.82	7.0	0.7	6.96	5.0	1.26	4.84	6.0	0.8	5.95
1500	5.1	1.22	4.95	7.0	0.6	6.97	5.5	1.2	5.37	7.0	0.75	6.96
2000	5.0	1.2	4.85	7.5	0.65	7.47	5.5	1.1	5.39	7.0	0.7	6.96

<Table. 4> Example of transformer impedance

Transformer Impedance	1 phase transformer					
	6.3kV/210V Oil Tr.			6.3kV/210V Mold Tr.		
Transformer capacity (VA)	ZT[%]	RT[%]	XT[%]	ZT[%]	RT[%]	XT[%]
10				14.9	14.9	0.268
20				14.0	14.0	0.503
30				14.8	14.8	0.523
50				13.6	13.6	0.494
75				11.0	11.0	0.558
100				8.87	8.85	0.562
200				7.70	7.68	0.571
300				5.75	5.69	0.619
500				5.08	4.97	1.05
750				5.05	4.92	1.16
1000				4.03	3.93	0.904
2000				4.55	4.50	0.637
3000				4.29	4.22	0.768
5000				3.26	3.18	0.725
7500				2.72	2.81	0.775
10000	2.5	2.07	1.40	2.33	2.18	0.823
15000	2.37	1.84	1.49	2.04	1.82	0.937
20000	2.57	1.76	1.87	1.90	1.60	1.02
30000	2.18	1.58	1.50			
50000	2.05	1.47	1.42			
75000	2.27	1.46	1.74			
100000	2.48	1.49	1.98			
150000	3.39	1.31	3.13			
200000	3.15	1.31	2.87			
300000	2.23	1.28	2.96			
500000	4.19	1.09	4.03			

<Table. 5> Example of cable impedance
(600 vinyl cable)

Cable dimension	Impedance of cable 1m (Ω)			
	Internal insulation wiring or cable of steel tube and duct	Internal vinyl tube wiring of steel tube and duct	Insulator wiring in building	Resistance (Ω) / cable 1meter
Ø 1.6mm				0.0089
Ø 2mm				0.0056
Ø 3.2mm	0.00020	0.00012	0.00031	0.0022
5.5mm ²				0.0033
8mm ²				0.0023
14mm ²				0.0013
22mm ²				0.00082
30mm ²	0.00015	0.00010	0.00026	0.00062
38mm ²				0.00048
50mm ²				0.00037
60mm ²				0.00030
80mm ²				0.00023
100mm ²				0.00018
125mm ²	0.00013	0.00009	0.00022	0.00014
150mm ²				0.00012
200mm ²				0.00009
250mm ²				0.00007
325mm ²				0.00005

<Remark1> At 60Hz, the reactance multiply 2 times itself, so 1/2 reactance of primary part can achieve 1B.

<Remark2> When the cable is parallelly 2 or 3ea, reactance and resistance can be calculated in the condition of 1/3 and 1/3 length cable.

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How to calculate short-circuit current value Various short-circuit

<Table.6> Impedance sample of bus and busduct (50Hz)

[$\times 10^{-4} \Omega /m$]

Ampere rating (A)	50Hz			60Hz		
	R	X	Z	R	X	Z
600	1.257	0.323	1.297	1.385	0.387	1.438
800	0.848	0.235	0.879	0.851	0.282	0.896
1000	0.641	0.185	0.667	0.645	0.222	0.682
1200	0.518	0.152	0.540	0.523	0.183	0.554
1350	0.436	0.129	0.454	0.443	0.155	0.469
1500	0.378	0.113	0.394	0.386	0.135	0.409
1600	0.360	0.107	0.375	0.367	0.128	0.389
2000	0.286	0.084	0.298	0.293	0.101	0.310
2500	0.218	0.065	0.228	0.221	0.078	0.235
3000	0.180	0.054	0.188	0.184	0.064	0.195
3500	0.143	0.042	0.149	0.146	0.051	0.155
4000	0.126	0.038	0.131	0.129	0.045	0.136
4500	0.120	0.036	0.125	0.122	0.043	0.130
5000	0.095	0.028	0.099	0.098	0.034	0.103

<Table.6> Impedance sample of Bus and busduct (50Hz)

[$\times 10^{-4} \Omega /m$]

Ampere rating (A)	50Hz			60Hz		
	R	X	Z	R	X	Z
600	0.974	0.380	1.045	0.977	0.456	1.078
800	0.784	0.323	0.848	0.789	0.387	0.879
1000	0.530	0.235	0.580	0.536	0.282	0.606
1200	0.405	0.185	0.445	0.412	0.222	0.468
1350	0.331	0.152	0.364	0.338	0.183	0.384
1500	0.331	0.152	0.364	0.338	0.183	0.384
1600	0.282	0.129	0.311	0.289	0.155	0.328
2000	0.235	0.107	0.259	0.241	0.128	0.273
2500	0.166	0.076	0.182	0.169	0.091	0.192
3000	0.141	0.065	0.155	0.144	0.078	0.164
3500	0.122	0.056	0.135	0.127	0.068	0.143
4000	0.110	0.051	0.121	0.113	0.061	0.126
4500	0.094	0.043	0.104	0.096	0.052	0.109
5000	0.082	0.038	0.091	0.084	0.045	0.096
5500	0.078	0.035	0.086	0.080	0.043	0.091
6500	0.068	0.028	0.074	0.071	0.031	0.077

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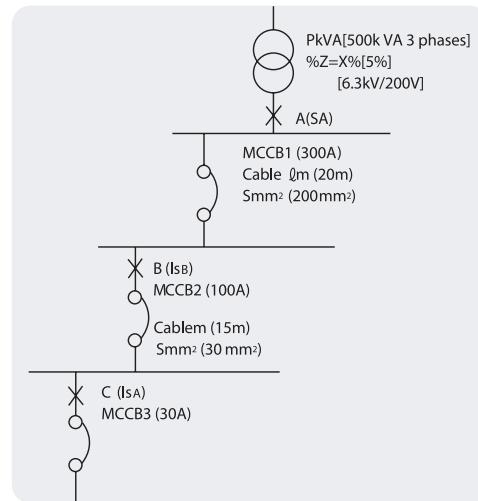
How to calculate short-circuit current value Calculation example

Using a certain graph, you can find and calculate the short-circuit current value which is at one position of network. No matter the condition of network is different, you can do the calculation through adjusting variables.

Graph note

- P coordinates – Transformer capacity (kVA)
- Is_1 coordinates – Short-circuit current value (kA)
- Is_2 coordinates – Short-circuit current value affected cable condition (kA)
- ① Line - % impedance of transformer (%)
- ② Line - Length of cable (m)
- ③ Line - Square mm of cable (mm²)
- ④ Line - Is_2 (kA)

(Remark) ④ line shows the length of hard vinyl cable (600V IV)



How to calculate short-circuit current value

(1) 3 phases transformer

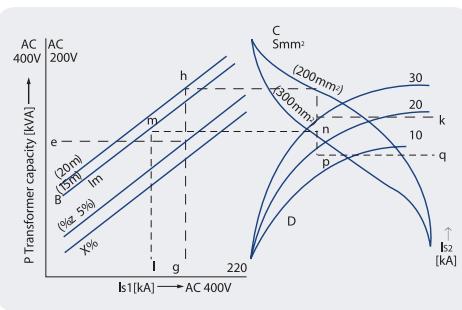
- ① Short-circuit current value at (A) where it is just below transformer. At P coordinates, find the coordinates value (g) of the cross point (f) which is from transformer capacity (e) and A line. Disregard primary part impedance of transformer.
- ② Find the short-circuit current value at Point B, C which are considered cable impedance.
 - At short-circuit current g (kA) of Is_1 coordinates, find the value (h) of B line
 - Move (h) to parallel direction of Is_1 , and find the cross point (i) to C line.
 - Move (i) to parallel direction of Is_2 , and find the cross point value (j) to D line (g), finally find (k) of Is_2

(2) 1 phase transformer

- ① Short-circuit current value where it is just below transformer. Find the value as same as that of 3 phase transformer and multiply it 3 times. (g'kA)
- ② Find the short-circuit current value where it is considered cable impedance.
 - Multiply 2/3 times to g' of Is_1 coordinates
 - Find the Is_2 value as same as that of 3 phase transformer and multiply it 3/2 times.

Remark

1. It's not considered the transformer contribution. Multiply 4 times the rated current of transformer in cases.
2. The real short-circuit current value is littler lower than its calculated value by the way we suggest because we take the rated voltage as AC200V, 400V. So the current value should be calculated in the consideration of stability
3. The calculated value is symmetrical real value.



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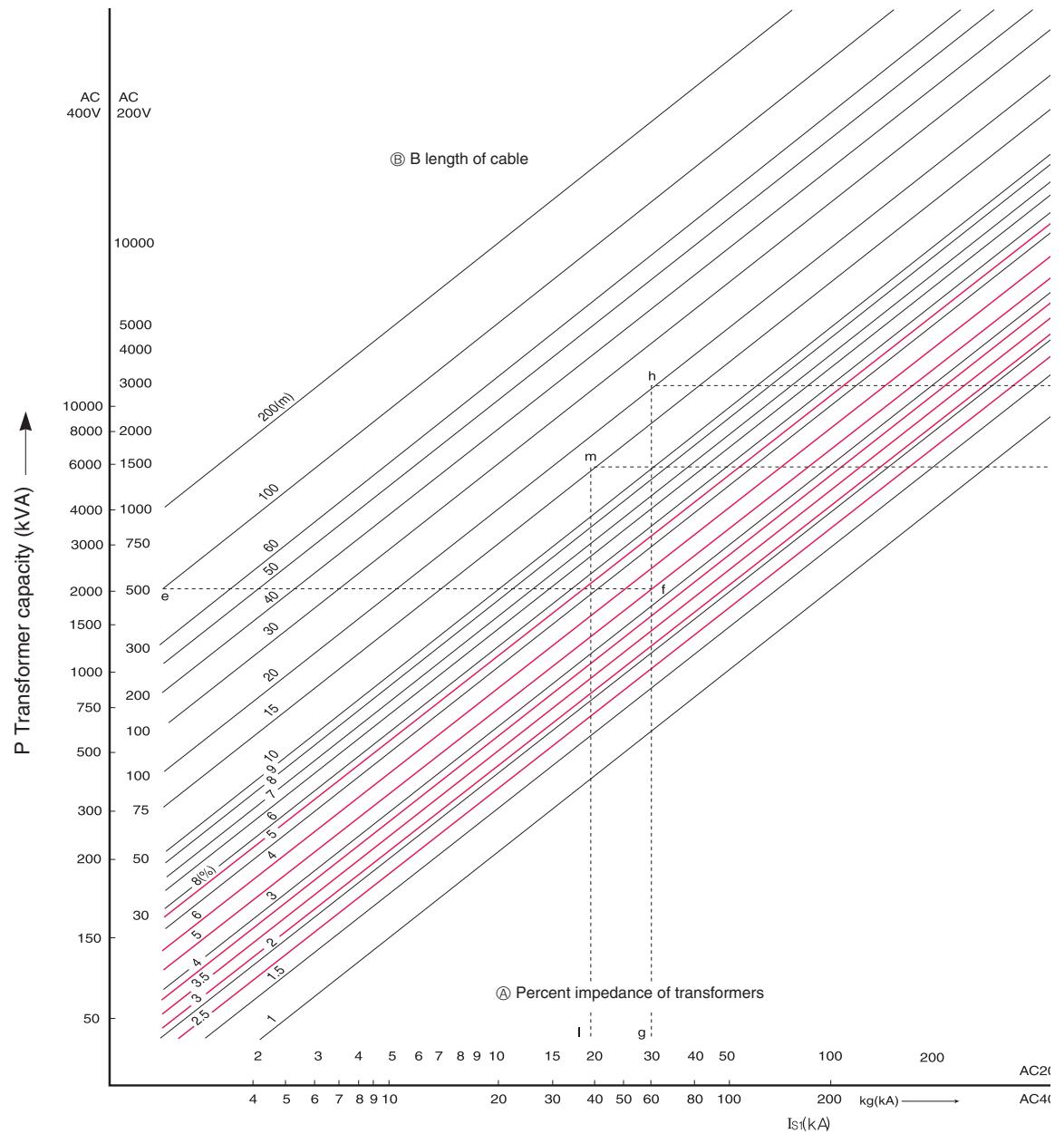
How to calculate short-circuit current value Calculation graph

(1) Short-circuit current value at point A (I_{SA})

- At P coordinates, find (f) which is the point which is to match transformer capacity 500kVA and A line. Then move (f) to I_{S1} direction and finally find (g).
- $I_{SA} = 29\text{kA}$ (g)

(2) Short-circuit current value at point B (I_{SB})

- Find value h of B line (20mm) at g (= 29kA) of I_{S1} coordinates
- Move h parallelly to the direction of I_{S1} , and find value I at the cross point with C line (200mm)
- Move I parallelly to the direction of I_{S2} , and find value j at the cross point with D line (g= 29kA)
- $I_{SB} = 19\text{kA}$ (k)

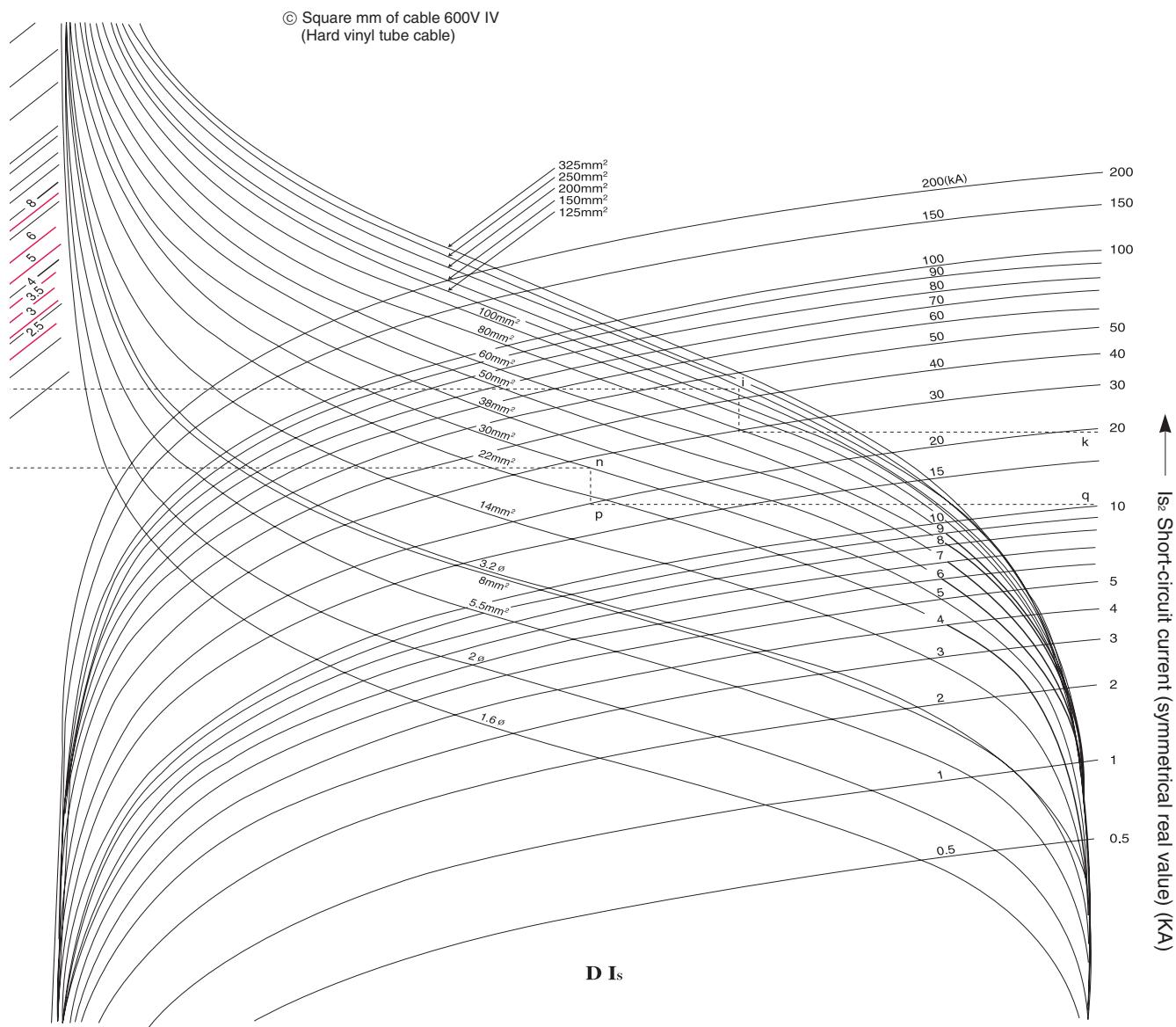


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(3) Short-circuit current value at point C (I_{sc})

- Find I_{s1} coordinates value (19kA) of short-circuit current value k (= 19kA) at Point B. and find cross point m between 19kA and B line.
- Move m parallelly to the direction of I_{s1} coordinates, and find the cross point n at C line (30mm).
- Move n parallelly to the direction of I_{s1} and find the cross point p of I_{s2} with D line.
- $I_{sc} = 10\text{kA}$ (g)



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Safety Instructions

- For your safety, please read user's manual thoroughly before operating.
- Contact the nearest authorized service facility for examination, repair, or adjustment.
- Please contact a qualified service technician when you need maintenance.
Do not disassemble or repair by yourself!
- Any maintenance and inspection shall be performed by the personnel having expertise concerned.

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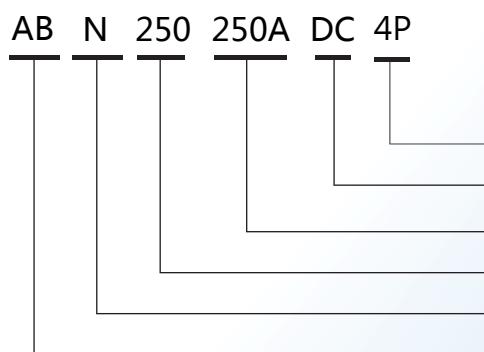
Specifications in this catalog are subject to change without notice due to continuous product development and improvement.

新产品介绍

ABN250-DC光伏专用直流断路器

ABN250-D系列光伏专用直流塑壳断路器，适用于额定电流250A及以下，直流额定电压1000V的光伏发电配电线路中。本断路器具有过载长延时保护、短路瞬时保护功能，可用于分配光伏电能和保护线路及用电设备免受过载、短路等故障的危害。

ABN250-D型塑壳断路器的额定分断能力为20kA，使用类别为A， $I_{cs}=100\%I_{cu}$ ，满足客户全部需求，可广泛应用于汇流箱、直流屏等设备当中。



- 6、极数
- 5、直流专用
- 4、额定电流
- 3、壳架电流
- 2、标准型
- 1、产品系列

技术资料

规格参数

额定电压 (V)	1000V DC	额定绝缘电压	1000V
额定电流 (A)	125A-160A-200A-250A	脱扣方式	热磁式
级数	2P、4P	电气寿命(次)	2000次
分断能力	20kA	额定冲击电压	8kV

标准认证

符合标准	IEC/EN60947-2 GB14048.2
通过认证	CCC

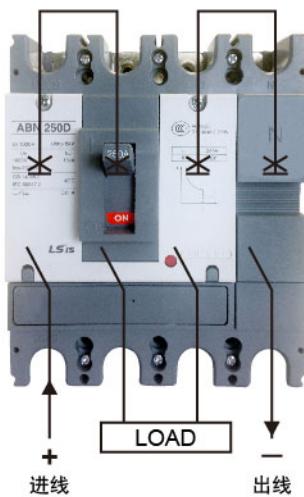
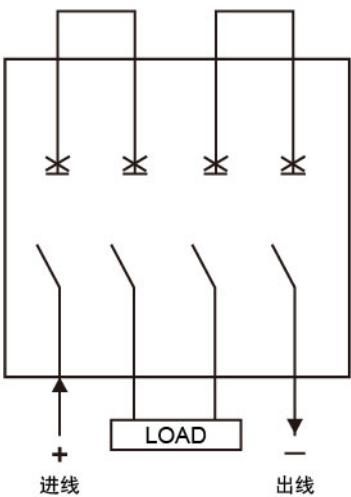
工作环境

降容	当环境温度超过40°C时，ABN产品的过载保护特性会随着温度发生很小的变化，需要对Ir进行整定，才能保证在高温环境下使用。 当海拔在2000米以上时，需考虑介电强度的改变和空气温度下降的因素，所以也需降容。
湿度	不超过50%
污染等级	3
环境温度 (°C)	-25 ~ +70
海拔 (m)	2000

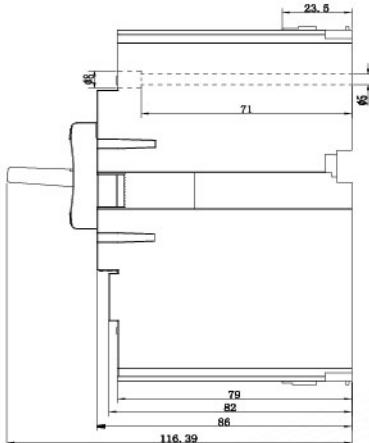
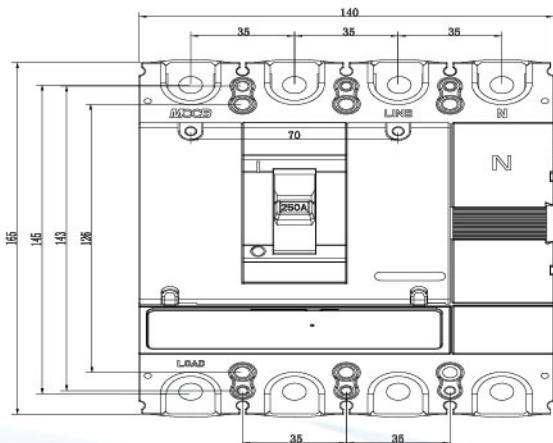
产品特点

安装方式	四极串联接线
产品附件	辅助触点（AX）、报警触点（AL）、分励脱扣器（SHT）
安装方向	水平或垂直
断点类型	双断点
产品极性	无极性
使用类别	A

产品接线图



外形尺寸



■ 国内网络

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